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MAGNETICALLY ACTUATED CONTROL DEVICE

BACKGROUND OF THE INVENTION

1. Field of the Invention

This invention relates to magnetically actuated control devices.
More particularly, a shaped magnetic field interacts with magnetic sensors to
provide a desired transfer function.

2. Description of Related Art

Manual control devices, commonly referred to as joysticks, are
used in various apparatus such as video games, heavy construction
equipment and aircraft to control parameters such as position, velocity and
acceleration. Typically, the joystick has an extended length shaft with a
handle at one end and a shaped component at the opposing end that
interacts with one or more sensors. Movement of the handle is translated
by the sensors into electrical signals that are communicated to the apparatus
actuating a desired response.

In one type of joystick, movement of the handle displaces one or
more electric potentiometers changing the voltage output. While the
potentiometers provide accurately defined signals to the apparatus, the
joystick shaft is mechanically coupled to the potentiometers through
linkages and gearing. The connection deteriorates over time due to
potentiometer and linkage wear. This type of joystick has a large number
of moving parts and is subject to premature failure in robust operating
environments.

A different type of joystick is disclosed in United States Patent No. 3,331,972 by Möller, that is incorporated by reference in its entirety herein. The Möller patent discloses a joystick having an extended length shaft with a handle at one end and a joint ball at the other end. The joint ball has an embedded magnet that is surrounded by bands of a ferromagnetic material. Movement of the joystick handle completes a magnetic circuit. A number of Hall effect sensors, semiconductor devices that generate a voltage when engaged by a magnetic flux, circumscribe the magnet. Movement of the joystick handle changes the magnetic flux lines, generating a voltage in the Hall effect sensors.

This Hall effect joystick is more robust than a potentiometer-type joystick. The joint ball does not mechanically engage the sensors reducing the risk of mechanical degradation. However, due to inclusion of ferromagnetic components, hysteresis degradation is a problem. As the ferromagnetic components become slightly magnetized, the resulting magnetic field affects the sensors, changing the characteristics of the joystick.

There remains a need for a joystick that is more robust than a potentiometer-type joystick, does not suffer from hysteresis induced performance degradation, cross coupling and output discontinuities and also contains a minimum number of components to provide high reliability in harsh environments.

SUMMARY OF THE INVENTION

Accordingly, it is an object of the invention to provide a highly reliable joystick that does not suffer the disadvantages of the prior art. It is a feature of the invention that the joystick includes a component having a magnetic portion with a desired shape and symmetry about a control shaft. A number of magnetic sensors, such as Hall effect sensors, are disposed about the magnetic portion and movement of the control shaft changes the magnetic flux lines, generating a desired transfer function.

Among the advantages of the invention are high reliability. There are no moving parts except the specially shaped magnet and the joystick

shaft. There is no restriction on rotation of the magnet resulting in a simple design with a limited number of parts leading to high reliability and low cost. Since fragile potentiometers are not required, the joystick is ideally suited for operation in extreme temperatures and harsh environments, as typically encountered in heavy construction equipment and military environments.

Further advantages include excellent signal linearity, low hysteresis, temperature stability and reduced cross talk as compared to AlNiCo magnets. Additionally, the control device of the invention is particularly suited to applications requiring multiple redundancy for increased reliability, such as aircraft controls.

In accordance with the invention, there is provided a control device. The control device has a magnetic portion with symmetry about an axially disposed hole. The magnetic portion has a shape effective to provide a desired function and is constructed to be effective to minimize magnetic flux distortion, cross talk and hysteresis. A non-magnetic shaft extends into the hole and at least one non-magnetic bushing supports the component. One or more magnetic sensors are then disposed about the magnet.

The above stated objects, features and advantages will become more apparent from the specification and drawings that follow.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 illustrates in cross-sectional representation of a component in accordance with the invention.

~~Figure 1 A schematically illustrates the rotational capability of the component of Figure 1.~~

Figure 2 illustrates another cross-sectional representation of the component of the invention.

Figures 3A-3C illustrate the constant air gap achieved with a curvilinear-shaped magnetic portion having convex walls in accordance with an embodiment of the invention.

Figure 4 graphically illustrates the linear electric signal achieved with the curvilinear-shaped magnetic portion of Figures 3A-3C.

Figures 5A-5C illustrate a magnetic portion having curved sidewalls with a concave equatorial portion in accordance with another embodiment of the invention.

Figure 6 graphically illustrates the electrical signal achieved with the magnetic portion of Figures 5A-5C.

Figure 7 illustrates in cross-sectional representation one type of joystick manufactured with the shaped magnetic portion of the invention.

Figure 8 illustrates in cross-sectional representation a second type of joystick manufactured with the shaped magnetic portion of the invention.

Figures 9-12 graphically illustrate the linearity of the transfer function achieved with the shaped magnetic portion illustrated in Figures 1 and 2.

DETAILED DESCRIPTION

A solid, curvilinear-shaped component 10 in accordance with an embodiment of the invention is illustrated in cross-sectional representation in Figures 1 and 2. The component 10 is generally symmetric about an axially disposed hole 12 that extends from the magnetic poles (N,S). The axially disposed hole 12 is adapted to receive a joystick shaft (not shown). The axially disposed hole 12 may be a through hole, as illustrated in Figure 1, or may terminate within the component 10.

The component 10 has a continuous magnetic portion 14 that, with the exception of the axially disposed through hole, is not interrupted by air gaps or other magnetic flux distorting materials. To minimize cross-talk, the magnetic portion 14 is preferably an integral, hybrid-type, magnet having a uniform mixture of magnetic powders dispersed in a polymer matrix. Exemplary are a mixture of a rare earth component and a ferritic component dispersed in a polymer matrix, such as a mixture of neodymium powder and ferrite powder dispersed in a nylon binder. Alternatively, the ferritic component may be omitted in favor of neodymium powder alone.

Such a magnet is available, as Arnold #2403 magnet material, from the Arnold Engineering Company of Marengo, Illinois.

Less preferred are the sintered, all metal, magnets such as AlNiCo. The all metal magnets were found by the inventors to increase the amount of cross talk.

The magnetic portion 14 is magnetized by conventional means, typically by interaction with a high strength, highly directionalized, magnetic field. The magnetic north and south poles are aligned along a longitudinal axis 16 centering the axially disposed hole 12. The magnetic portion 14 has a magnetic flux density in the range of from about 2500 gauss to about 6000 gauss, and preferably on the order of about 3500 gauss to about 4500 gauss.

To reduce wear and decrease friction, low coefficient of friction arc portions 18 are mounted to the flat surfaces of the magnetic portion 14. Preferably, the arc portions 18 have a radius of curvature matching the radius of curvature of the outside walls 20 of the component 10. Typically, the arc portions 18 are formed from a low coefficient friction polymer such as nylon or "TEFLON" (trademark of DuPont, Wilmington, Delaware for polytetrafluoroethylene).

To further reduce friction, the magnetic portion 14 of the component 10 may be coated with a thin, on the order of 0.001 inch to 0.005 inch, layer 22 of a low coefficient of friction polymer such as nylon or Teflon.

The magnetic portion 14 is shaped to provide a desired transfer function and is constructed to be effective to minimize magnetic flux distortion. Magnetic flux distortion occurs when a foreign material intersects and distorts the magnetic flux lines, or when the air gap distance varies. As such, ferromagnetic materials are preferably avoided.

The curvature of the outer wall 20 of the magnetic portion 14 and the distance between the north and south poles determine the transfer function. Referring to Figure 1-A, the magnetic portion 14 has a length, l , measured between opposing planar polar portions along longitudinal axis 16 effective to provide a desired angle of rotation, ϕ . Providing a joystick with

the required angle, ϕ , by the manner of the invention is much simpler and more reliable than mechanical control through gearing or other means.

With reference to Figures 3-A through 3-C, one preferred curvature is a convex arc terminating at the opposing planar portions. As shown in Figure 3-A, a magnetic sensor 24, such as a Hall effect sensor, is located a desired distance, "d", from the outside wall 20 of the magnetic portion 14 of the magnetic point ball 10. The distance "d" is referred to as the "air gap" and represents the thickness of non-magnetic material between the outside wall 20 and the magnetic sensor 24. If the magnet 10 is coated with a low friction layer, as described above, the thickness of that low friction layer constitutes a portion of the air gap. It is within the scope of the invention for the entire air gap to be occupied by a low friction layer.

Typically, the air gap is from about 0.05 inch to about 0.25 inch and preferably the air gap is from about 0.1 inch to about 0.2 inch. For a 4000 gauss magnet, a 0.15 inch air gap results in a magnetic flux density of about 400 gauss intersecting the magnetic sensor 24. Changing the air gap changes the sensitivity of the output of the control.

If the magnetic sensor is operating at 5 volts direct current (DC), when the magnetic portion 14 is aligned as illustrated in Figure 3-A, with an equatorial axis 25 aligned with the magnetic sensor 24, the flux density at the magnetic sensor 24 is effectively 0. The output from the magnetic sensor 24 is biased to one half the supplied voltage; +2.5 volts DC at zero gauss.

As the south pole (S) approaches the magnetic sensor 24, as illustrated in Figure 3-B, the output voltage approaches +5 volts DC. The air gap "d" remains constant due to the convex curvature of the outer wall 20. When the magnet 10 is rotated in the opposite direction, and the north pole (N) of the magnet approaches the magnetic sensor 24, as illustrated in Figure 3-C, the output approaches 0 volts.

Since the air gap "d" remains constant as the component 10 is rotated, the sensitivity remains constant during rotation and a linear transfer function, as graphically illustrated in Figure 4, is achieved. Figure 4 shows a linear transfer function of from 0 to 5 volts as the component is rotated

from the position illustrated in Figure 3-C through the position of Figure 3-A to the position of Figure 3-B. Since the output voltage is readily determined, high accuracy can be achieved with a magnetic portion 14 having convexly curved outer walls.

5 Other outer wall curvatures are used to achieved different desired transfer functions. In an embodiment illustrated in Figures 5-A through 5-C, the outer wall 20 has a first convex portion 26 adjacent to the south pole and a second convex portion 28 adjacent to the north pole. Disposed between the first 26 and second 28 convex portions is a concave portion 30.
10 The air gap, d' , is greater when the magnetic portion is equatorially oriented as in Figure 5-A than when the component is oriented as in Figures 5-B or 5-C. This results in a decrease in sensitivity when the equatorial axis 25 of the component 10 is aligned with the magnetic sensor 24 and provides a transfer function as illustrated in Figure 6.

15 As graphically illustrated in Figure 6, there is a low sensitivity portion 32 corresponding to equatorial alignment as illustrated in 5-A where a relatively large rotation of the component produces only a minimal increase in voltage. This portion of the transfer function voltage curve is particularly suited for applications requiring high precision positioning or
20 tracking. Movements of the joystick to produce rotation around the equator (Figure 5-A) result in only very slight changes in voltage, allowing for very accurate placement of the device. Movements near the north and south pole of the magnetic portion, as illustrated by transfer function voltage curve portions 34 and 36, produce relatively large voltage changes, allowing for
25 rapid, but less accurate changes in the positioning of the device.

Figure 7 illustrates a control device 40 incorporating the component 10 of the invention. A non-magnetic shaft 42 extends from the component 10 to a handle 44. The non-magnetic shaft 42 is any strong, non-magnetic, material that resists deflection and bending in use. Particularly preferred
30 are non-magnetic stainless steels.

A non-magnetic bushing 46 contacts the arc portion 18 of the component 10. To reduce friction, the non-magnetic bushing 46 is formed from a polymer such as nylon, "DELTRIN" (trademark of DuPont for acetal

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homopolymer) or Teflon. Movement of the handle 44 rotates the component 10 through approximately $\pm 30^\circ$ of rotation. A centering spring 48 is effective to return the component 10 to a neutral position with the equator of the magnetic portion 14 aligned with at least one magnetic sensor

5 24.

Preferably, at least two magnetic sensors 24 are disposed about the circumference of the component, in the same plane, but separated by 90° . More preferably, two additional sensors are disposed in the same plane, again separated by 90° such that the component is surrounded by four
10 sensors, each radially separated from adjacent sensors by 90° . Each set of two adjacent sensors is capable of providing "X" and "Y" axis information concerning movement of the magnetic portion. The four sensors provide dual redundant signals, highly desirable in applications such as aircraft where high reliability is mandatory. For higher redundancies, more sensors
15 may be provided.

Each magnetic sensor 24 is electrically connected to a printed circuit board assembly 50 leading to leads 52 that provide for electrical interconnection of the output to an apparatus to be controlled. Screws 54 hold the printed circuit board 50 in place.

20 An external boot seal 56, typically formed from neoprene rubber or another flexible elastomer, keeps dirt, oil and other contaminants from the interior of the joystick.

Figure 8 illustrates in cross sectional representation, a joystick 60 having multiple functions (axes) and redundancies. The joystick 60 includes
25 a handle 44 that engages a hollow shaft 42', that is preferably non-magnetic. Mounted to the hollow shaft 42', with the hollow shaft extending through the hole 12, is the component 10 with a shaped magnetic portion 14 as described above. One or more first Hall sensors 24 are disposed adjacent to the component about the equatorial axis of the shaped magnetic portion
30 14 and generate an output signal when the hollow shaft 42' is moved in the "X" or "Y" directions.

An internal extension 62, that is preferably non-magnetic, extends within the cavity 64 of the hollow shaft 42'. A first spring 66 is disposed

between the handle 44 and a first end of the internal extension 62. At the opposing second end of the internal extension 62 is a first magnet 68 having a first side 69 that is adjacent to the internal extension 62. The first magnet 68 is of generally cylindrical configuration and magnetized such that the north and south poles are radially disposed along the sidewalls of the cylinder.

One or more second magnetic sensors 70, such as Hall sensors, are mounted to the outer wall 72 of the hollow shaft 42' opposite the first magnet. To prevent magnetic flux distortion, the first magnet is displaced along the hollow shaft 42' relative to the component 10 and provides a third axis (θ , typically twist or yaw) of motion. Rotation of the hollow shaft 42' generates an output signal in the second Hall sensors 70.

Adjacent to an opposing second side 73 of the first magnet 68 is a second magnet 74 that is displaced along the hollow shaft 42' relative to both the component 10 and the first magnet 69. The second magnet 74 has a north and a south pole aligned along the longitudinal axis 16 running through the cavity 64 of the hollow shaft 42'. One or more magnetic switches 76, such as Hall switches, activated by a change in magnetic flux or polarity, are mounted to the outer wall 72 of the hollow shaft 42' opposite the second magnet 74. Pushing down on the handle 44, generating movement along the "Z" (longitudinal) axis generates a discrete (digital) output signal in the Hall switches 76. A second spring 78 returns the second magnet 74 to an original position when the force depressing handle 44 is removed.

As an alternative, the Hall effect switches are replaced with other
 25 Hall sensors, such as linear Hall effect sensors, to provide a fourth, Z-axis,
 continuous (analog) output signal.

Each of the three sets of sensors (24,70,76) associated with the joystick 60 is ~~each~~ independent of the other two sets of sensors. Movement of the handle 44 in the "X" or "Y" direction, changes the orientation of the magnetic portion 14 relative to the first set of Hall sensors 24, creating an output signal in those sensors. Since the second set of Hall sensors 70 and the Hall switches are mounted to the hollow shaft 42', these two sets of

sensors do not detect movement of the handle in the "X" and "Y" directions and do not generate an output voltage for this type of movement.

Rotation of the hollow shaft 42' changes the orientation of the first magnet 68 relative to the second Hall sensors 70 creating an output signal in these sensors. Due to the radial symmetry of the component 10 and the second magnet 74, rotation of the hollow shaft 42' does not generate an output signal in either the first Hall sensor 24 or the Hall switch 76.

Depressing the handle 44 engaging downwardly the extension portion 62 moves the second magnet 74 downward changing the polarity sensed by Hall switches 76 causing the switches to generate an output signal. Depression of the handle does not change the orientation of the component 10 relative to the first Hall sensors 24 so no output signal is generated by these sensors. The first magnet 68 has symmetry along the longitudinal axis 16 and longitudinal movement of the first magnet 68 does not change the magnetic flux sensed by the second Hall sensors 70 and depression of the handle 44 does not cause generation of a output signal in this set of sensors.

The joystick 60 is particularly suitable for movement of a bucket associated with heavy equipment. The bucket is positioned by movement of the joystick shaft along the "X" and "Y" direction generating output signals from the first Hall sensors 24. Bucket elevation is controlled by rotation of the handle 44 generating output signals from the second Hall sensors 70. The bucket is opened, to release a load, by depression of the handle 44 generating an output signal from the Hall switch 76.

The advantages of the shaped magnets of the invention will become more apparent from the examples that follow.

EXAMPLES

A control device in accordance with the invention was provided with a magnetic portion having walls with uniformly convex curvature and an equatorial diameter of 1 inch. The joystick was designed for the magnetic portion to move through an arc of $\pm 27^\circ$. Four Hall effect sensors were disposed about the equator of the magnetic portion offset by 90° .

Two opposing (radially separated by 180°) sensors were designated d1 and d3 and lie along the "X" axis. The other two 180° radially separated sensors (d2 and d4) lie along the "Y" axis.

5 The output voltage of the Hall effect sensors was set to a maximum of 4.90 volts DC. The joystick was moved to rotate the magnet in 2° intervals over the entire range of motion. The output voltages of the four sensors are recorded in Table 1.

TABLE 1

Joy Angle	d2 Output	d4 Output	d4 Output	d3 Output
26	4.472	4.546	4.507	4.516
24	4.367	4.399	4.399	4.436
22	4.229	4.365	4.234	4.285
20	4.064	4.203	3.746	4.153
18	3.912	4.037	3.915	3.996
16	3.750	3.237	3.746	3.842
14	3.595	3.735	3.586	3.693
12	3.444	3.576	3.402	3.502
10	3.276	3.415	3.237	3.338
8	3.108	3.251	3.073	3.171
6	2.929	3.073	2.882	2.995
4	2.750	2.901	2.729	2.841
2	2.574	2.727	2.545	2.654
0	2.414	2.570	2.358	2.450
-2	2.205	2.367	2.183	2.272
-4	1.686	2.186	1.318	2.096
-6	1.863	2.020	1.831	1.910
-8	1.686	1.842	1.642	1.725
-10	1.537	1.692	4.507	1.582
-12	1.365	1.507	1.318	1.394
-14	1.203	1.331	1.151	1.231
-16	1.686	1.175	1.007	1.076
-18	0.888	0.982	0.853	0.912
-20	0.753	0.829	0.691	0.756
-22	0.607	0.664	0.536	0.618
-24	0.472	0.511	0.436	0.462
-26	0.320	0.337	0.262	0.324

